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Novel railpad design using a multi-level digital twin method

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COMATEC, HEIG-VD/HES-SO, Switzerland



Novel rail pad design methodology

“Novel Rail Pad” project funded by Swiss Federal Office for Environment (FOEN)

Optimized rail pads to:

1. Reduce the sound emission of the tracks.
2. Improve ballast protection, reduce maintenance.

Modelling:

To achieve this goal several models have been developed to predict the effect of the rail pad on:

- the rail, sleeper & ballast vibrations level (FRF & TDR).
- the rail-borne sound emissions.
- the ballast loading & degradation (relative settlement rate).

Optimization:

- Single/multi material pad with tailored materials properties & complex geometry
- Optimal frequency dependent pad stiffness and damping:
 - Soft at low frequencies for ballast protection
 - Stiff & high damping at high frequencies to reduce noise

=> need to use detailed 3D finite elements models and 3D constitutive models for the pads material to account for shear / confinement effects.



Digital twin approach “level 1”:

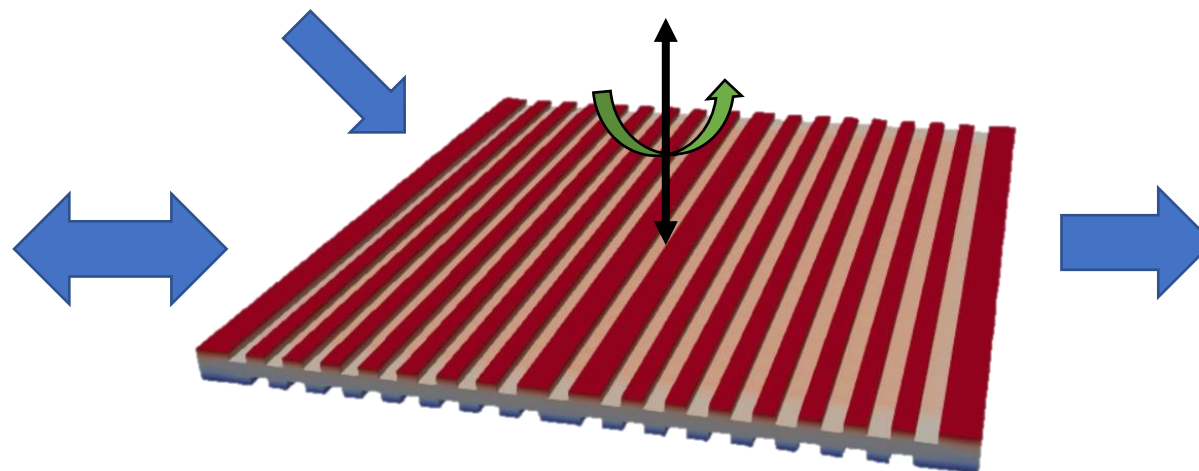
Quick design /evaluation of the pad dynamic response for optimum track performance



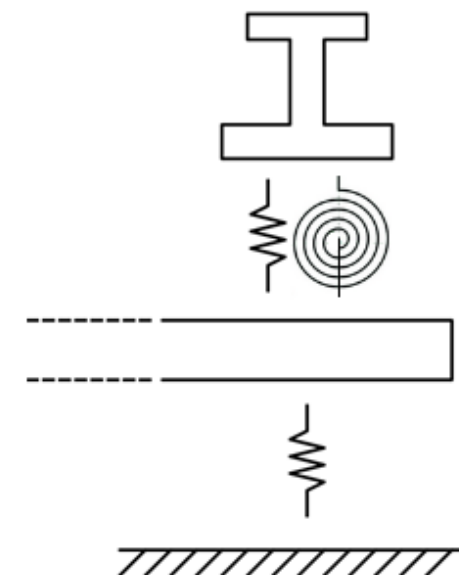
Experimental
validation

DMA material properties
 $E, \tan(\delta) = f(\omega, T)$

3D geometry of the pad
(FE mesh)



Pad Stiffness & Damping model
 $\mathbf{K}(\omega)$ and $\mathbf{\tan}(\delta(\omega))$ computed for 4 DOF
(Compression, rotations and shear)

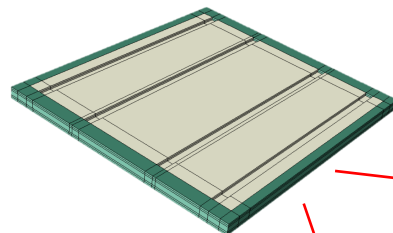


Fast semi-Analytical track model:
FRF & TDR, sound radiation

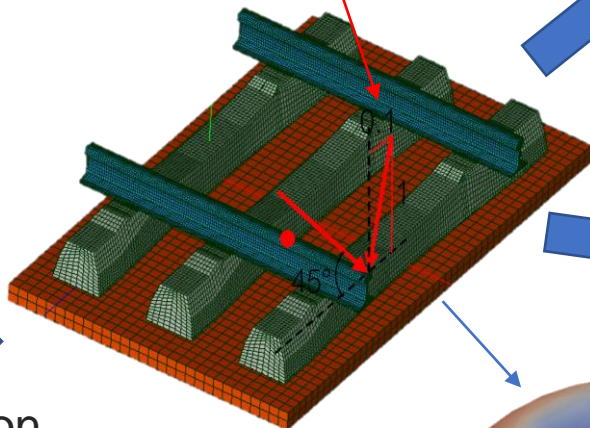
Digital twin approach “level 2”:

Detailed 3D optimization of the pad design

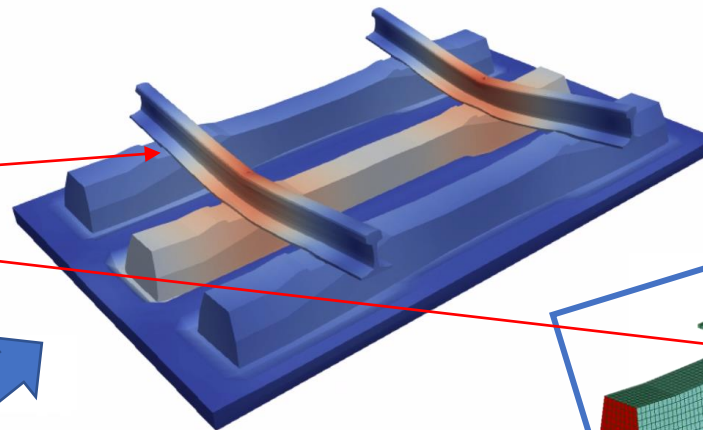
pad design
(3D FEM +
materials)



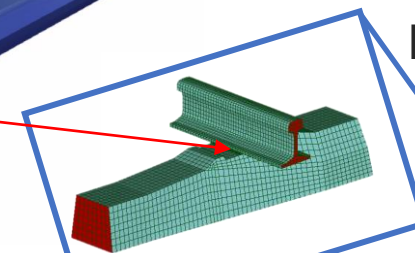
Three sleepers model



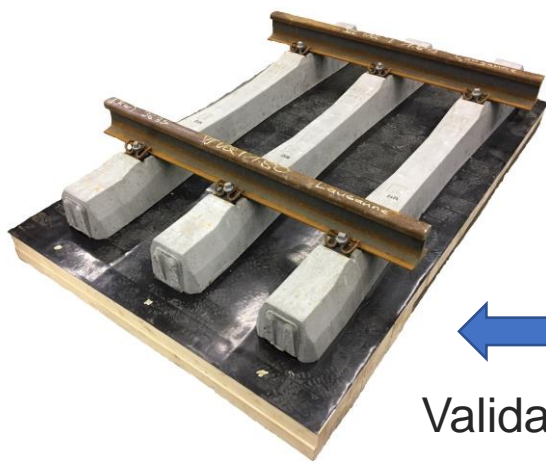
Impulse model



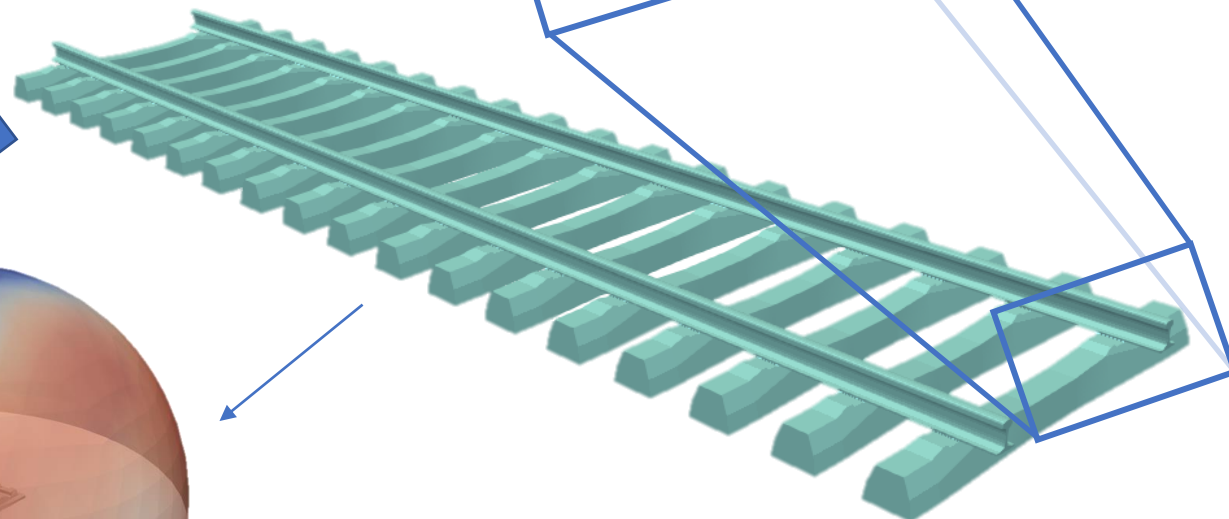
Macro element



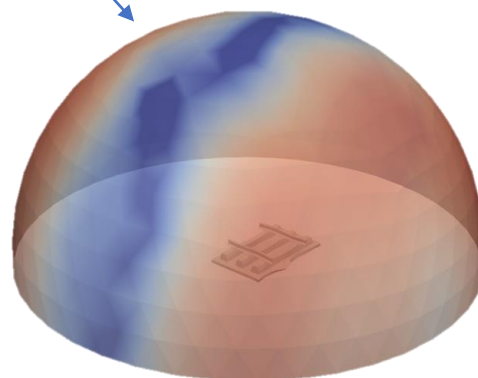
Experimental unit cell



Validation



Large scale track using
dynamic substructuring



Sound pressure levels estimated with either
the three sleepers model or the multi-sleeper model

Digital Twin Level 1 : first design loop

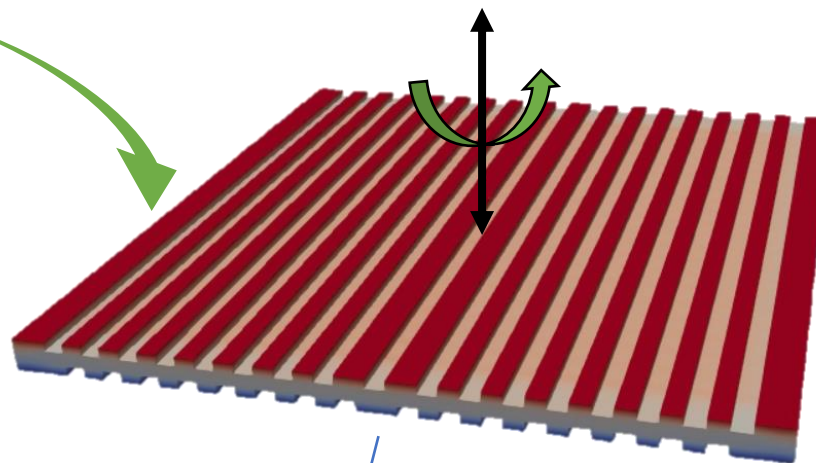
Pad Stiffness & Damping model

Experimental

DMA material properties



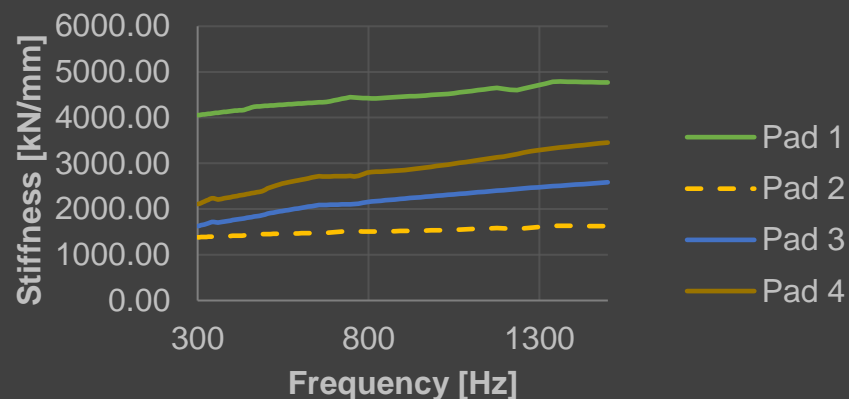
Numerical models



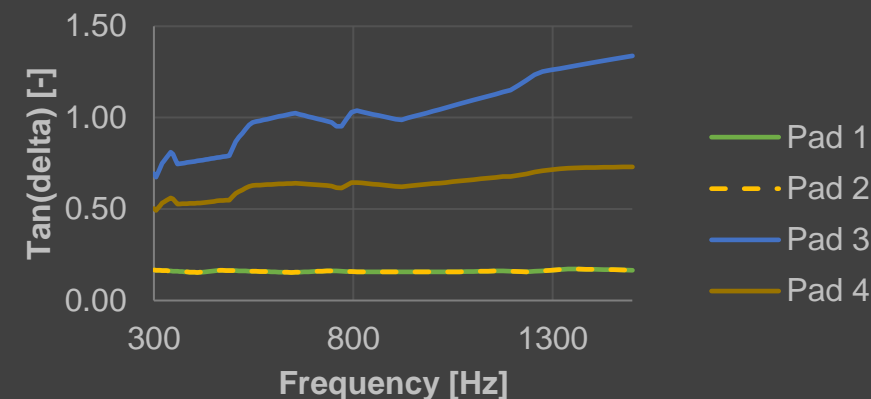
Pad Stiffness & Damping model
K(ω) and **tan(δ(ω))** computed for 4 DOF
(Compression, rotations and shear)
Compute the Acoustic index of a pad

$$I_a = \frac{k_{pad}'' [1000 \text{ Hz}]^{0.365} \cdot \tan(\delta)_{pad} [1000 \text{ Hz}]^{0.347}}{k_{EVA}'' [1000 \text{ Hz}]^{0.365} \cdot \tan(\delta)_{EVA} [1000 \text{ Hz}]^{0.347}}$$

Compression stiffness real part

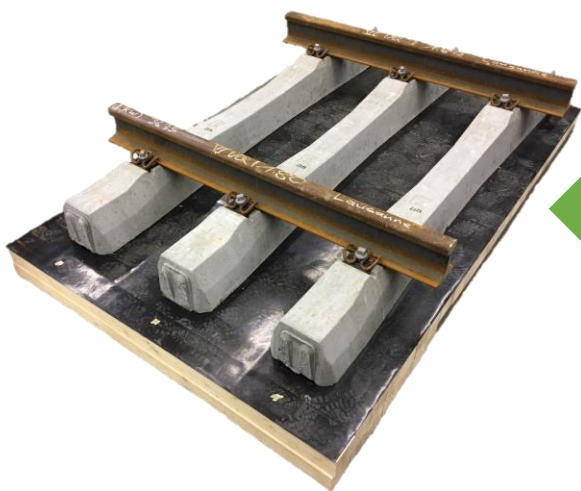


Tan(delta) - Damping

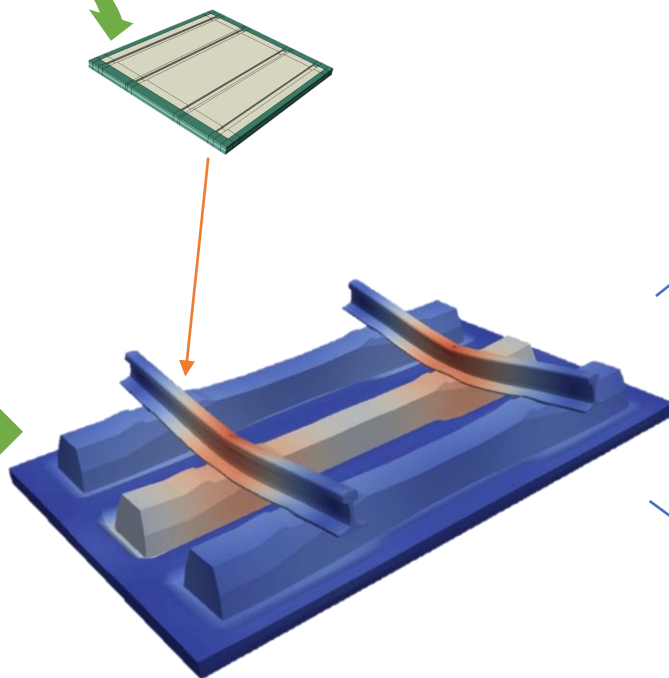


Experimental

DMA material properties

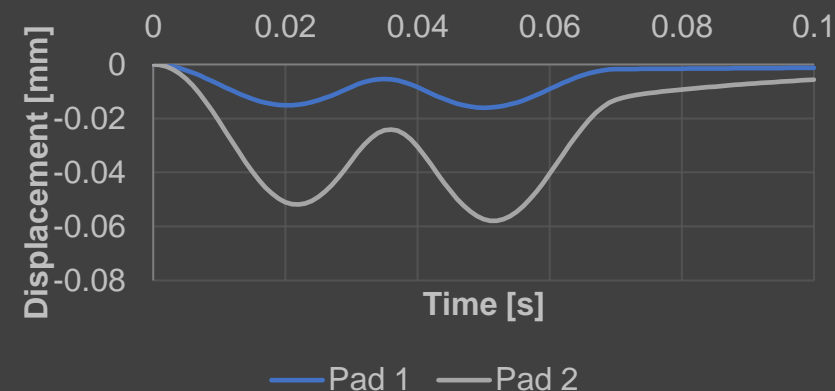
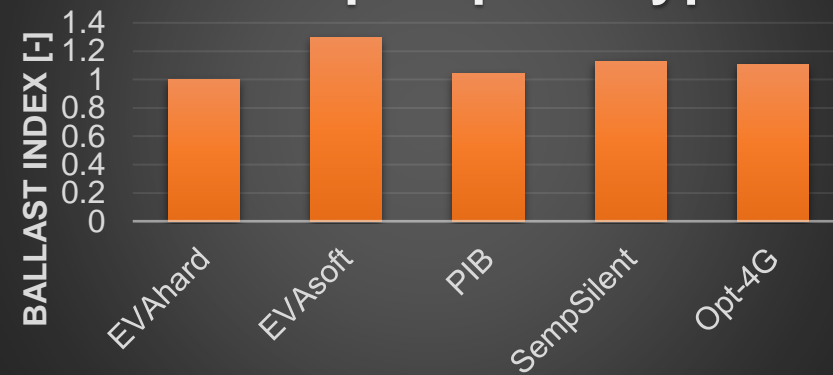


Numerical models



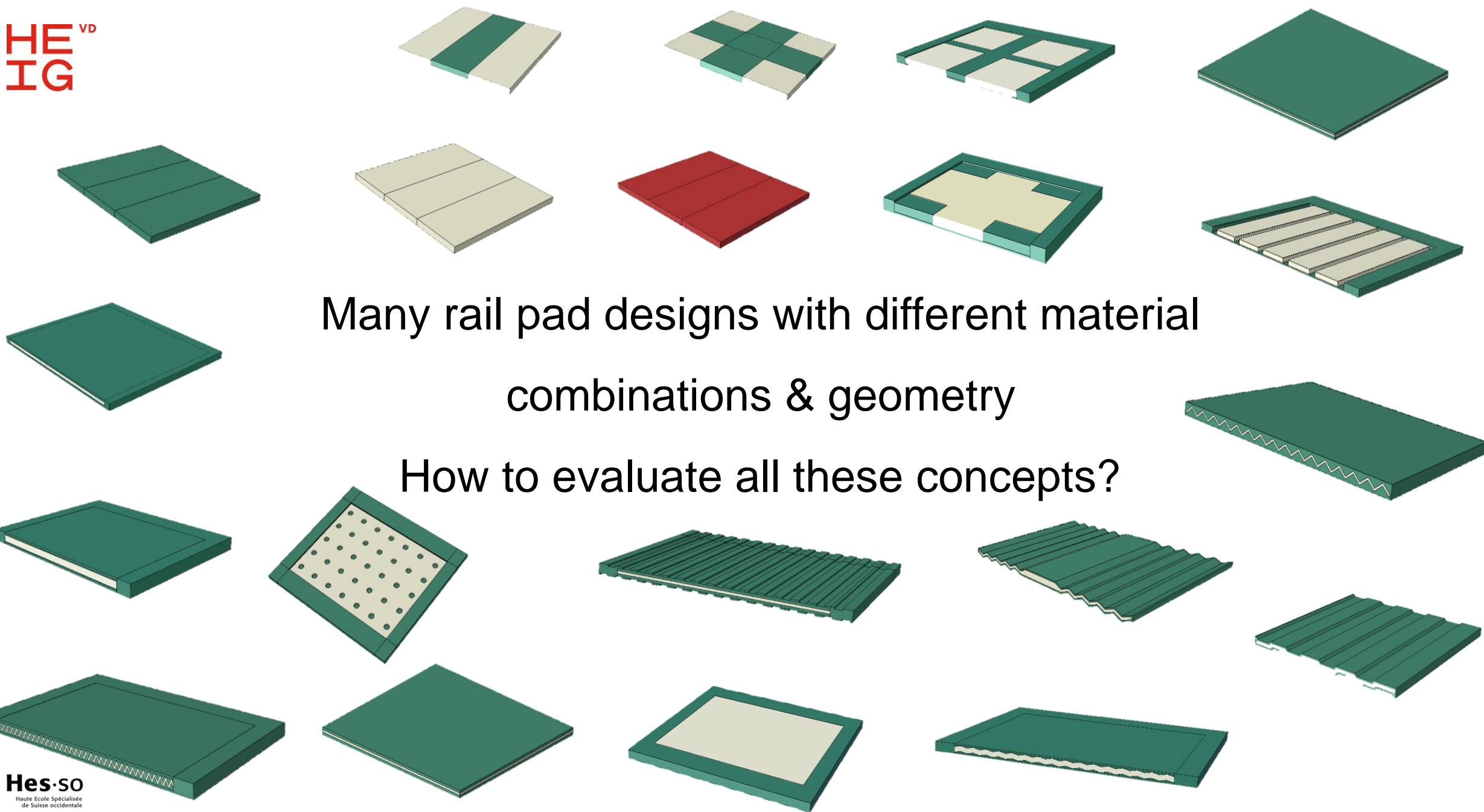
Impulse model
Reproduction of a bogie pass-by,
compute the ballast and pads
solicitation.

$$I_b = \frac{N_{pad}}{N_{EVA}}, \quad N = \exp_{10} \left(\sqrt{S \frac{160}{\sigma} \frac{47}{K_s}} + 2.4 \right)$$

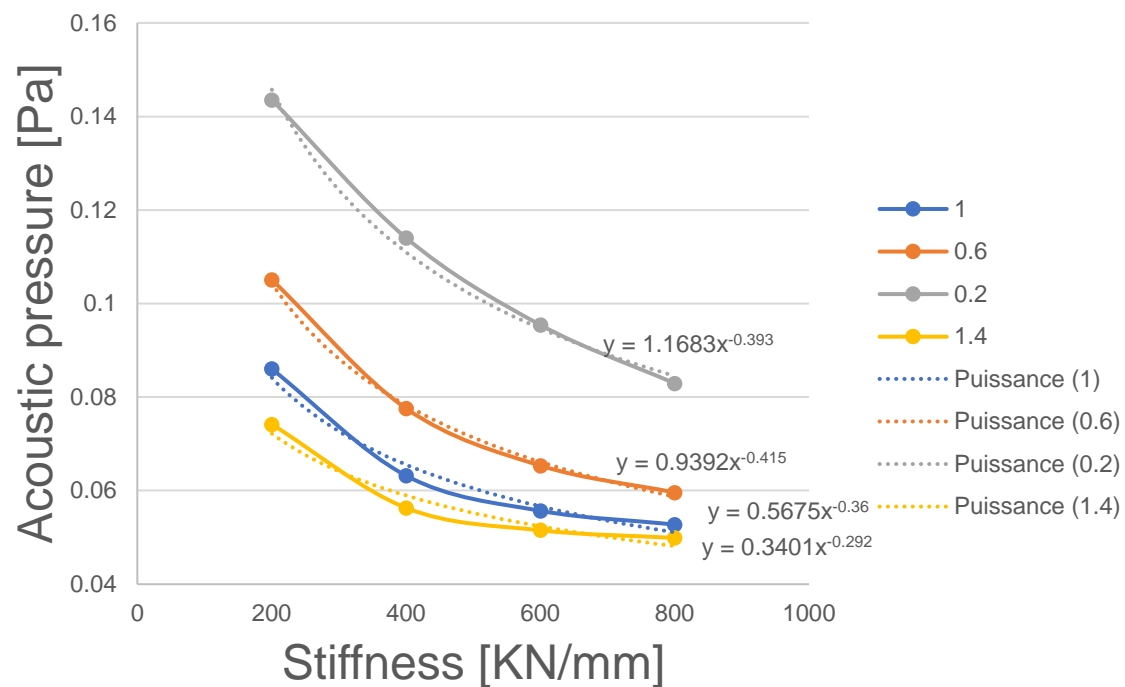
Relative displacement between the rail and
the sleeper.Ballast Index for
various pad prototypes

Many rail pad designs with different material combinations & geometry

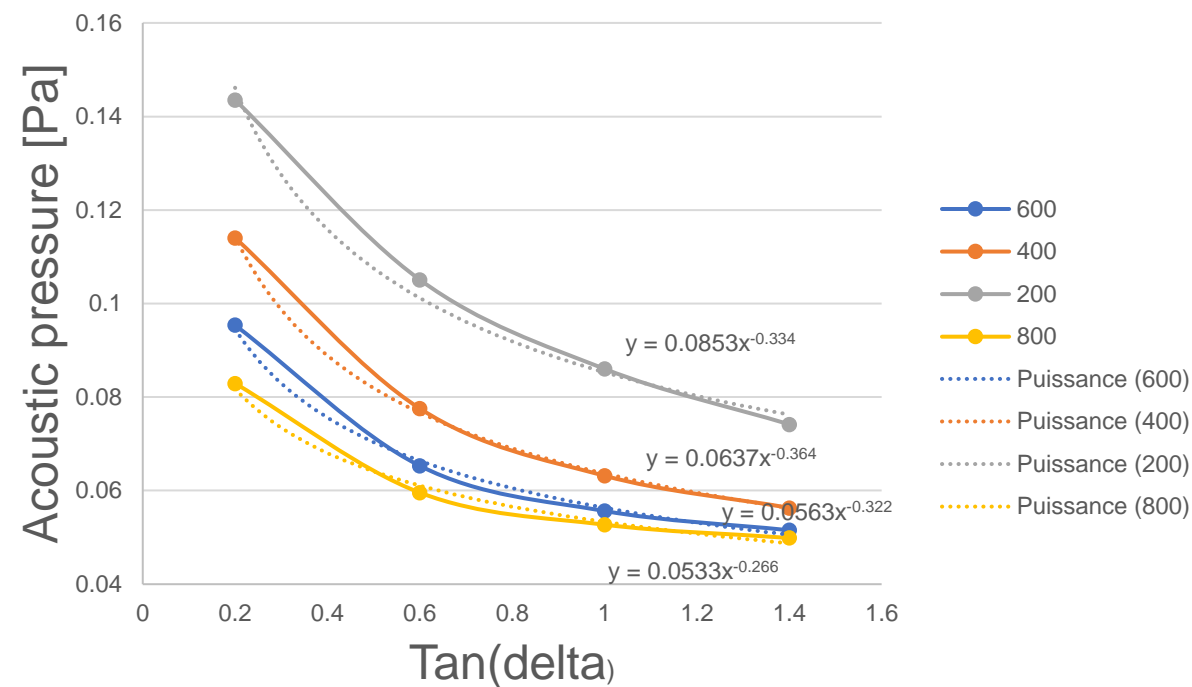
How to evaluate all these concepts?



Acoustic pressure in function of the stiffness



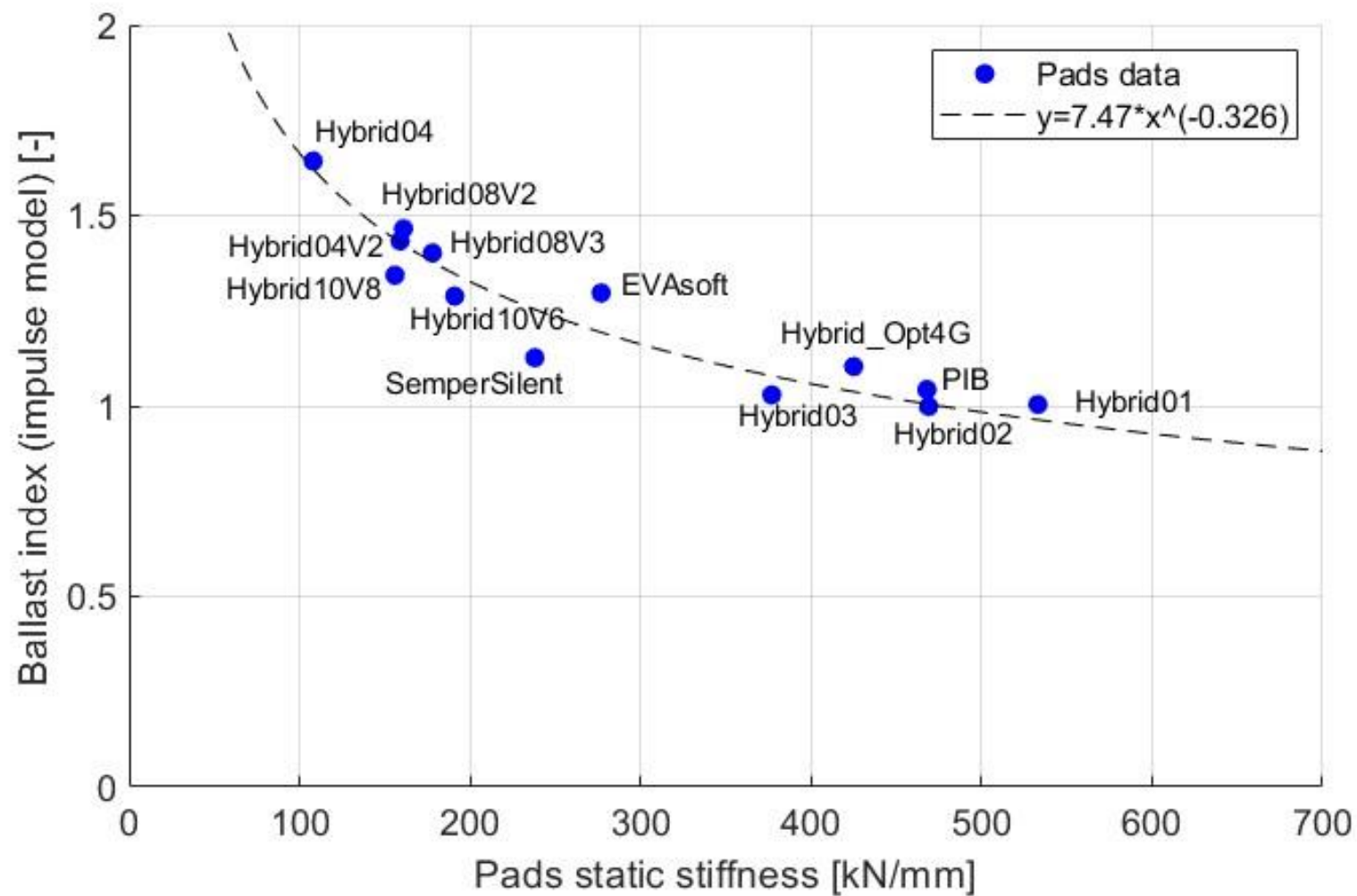
Acoustic pressure in function of the tan(delta)



$$\text{Noise reduction} \sim K'^{0.365} * \tan(\delta)^{0.347}$$

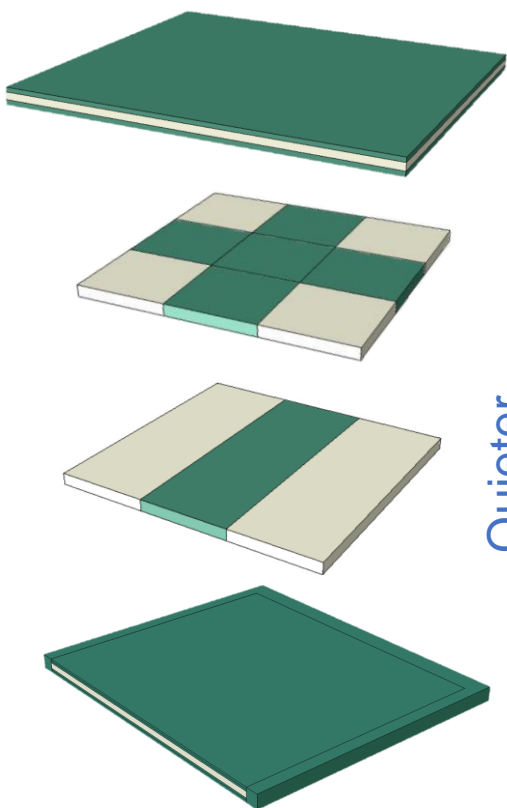
where K' and $\tan(\delta)$ are the dynamic stiffness and damping are the simulated pad properties at 1000hz

Ballast Index

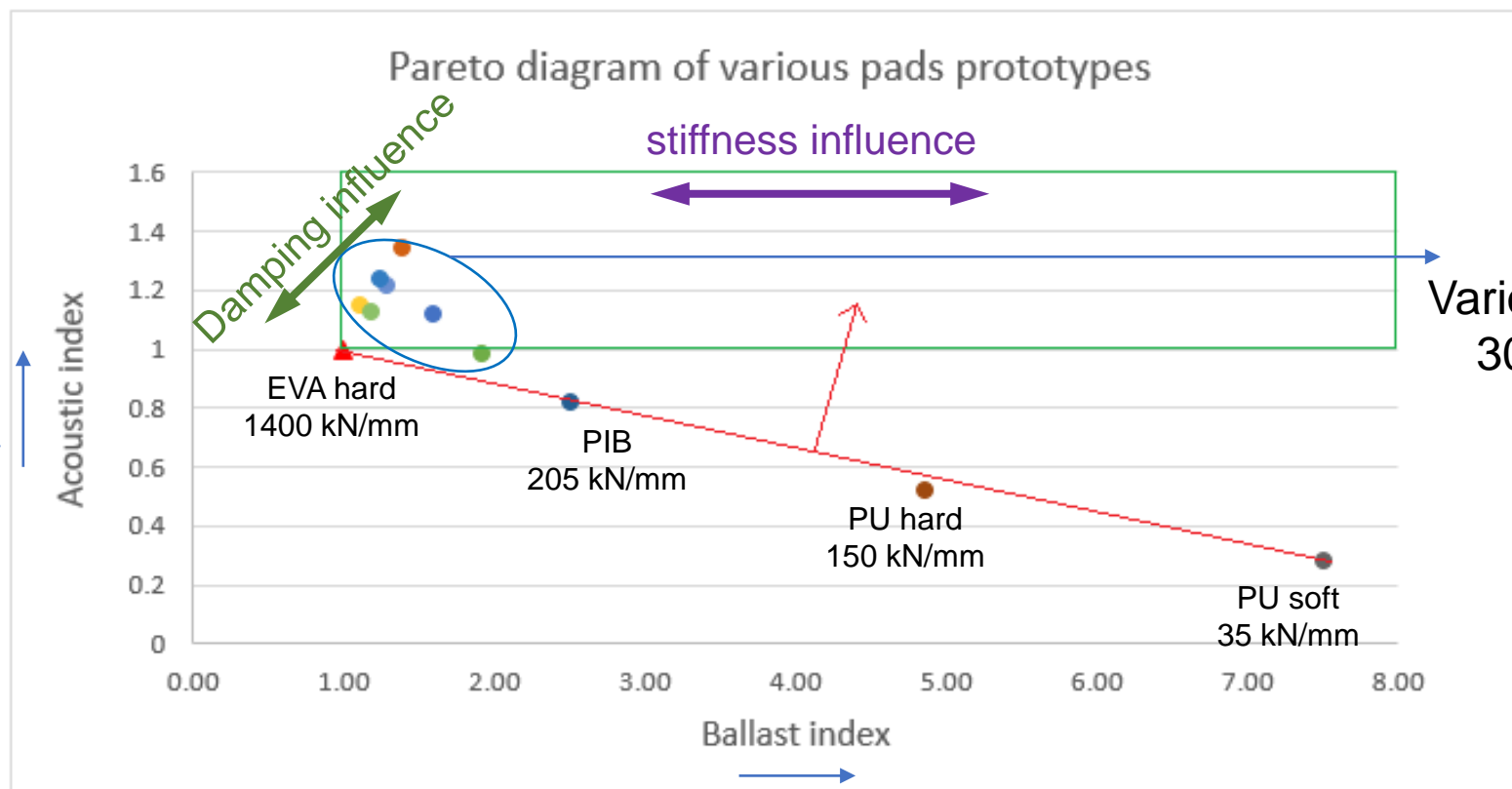


$$I_b = \frac{N_{pad}}{N_{EVA}}, \quad N = \exp_{10} \left(\sqrt{S \frac{16047}{\sigma K_s}} + 2.4 \right)$$

Noise vs Ballast protection optimization: First design loop



Quieter ↑



Various pad properties
300 – 800 kN/mm

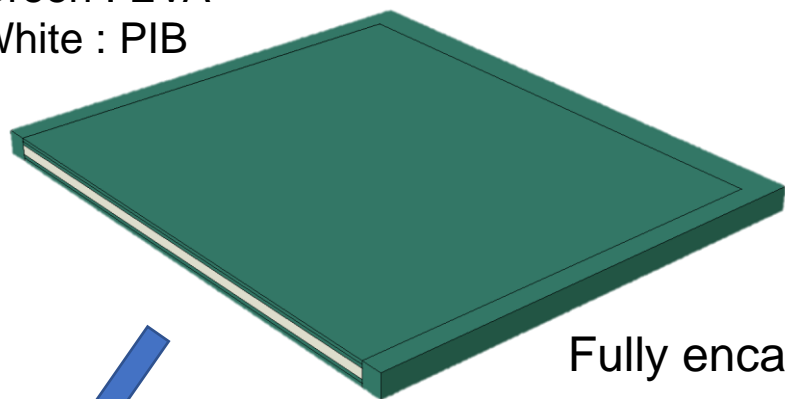
Less maintenance →

$$I_a = \frac{k_{pad}'' [1000 \text{ Hz}]^{0.365} \cdot \tan(\delta)_{pad} [1000 \text{ Hz}]^{0.347}}{k_{EVA}'' [1000 \text{ Hz}]^{0.365} \cdot \tan(\delta)_{EVA} [1000 \text{ Hz}]^{0.347}}$$

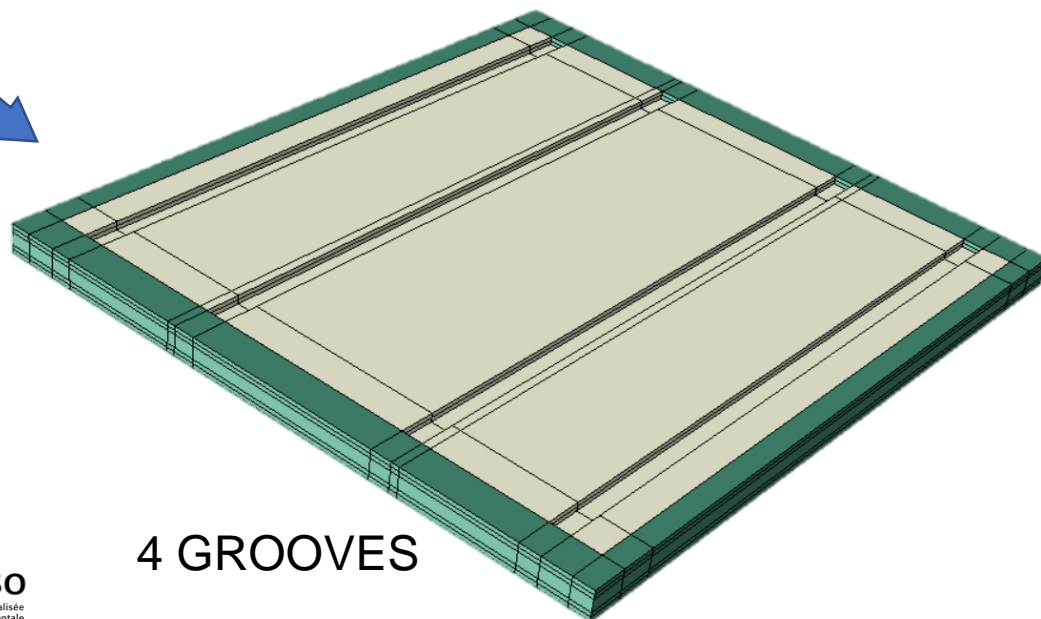
$$I_b = \frac{N_{pad}}{N_{EVA}}, \quad N = \exp_{10} \left(\sqrt{S \frac{160}{\sigma} \frac{47}{K_s}} + 2.4 \right)$$

Hybrid Design EVA-PIB Evolution

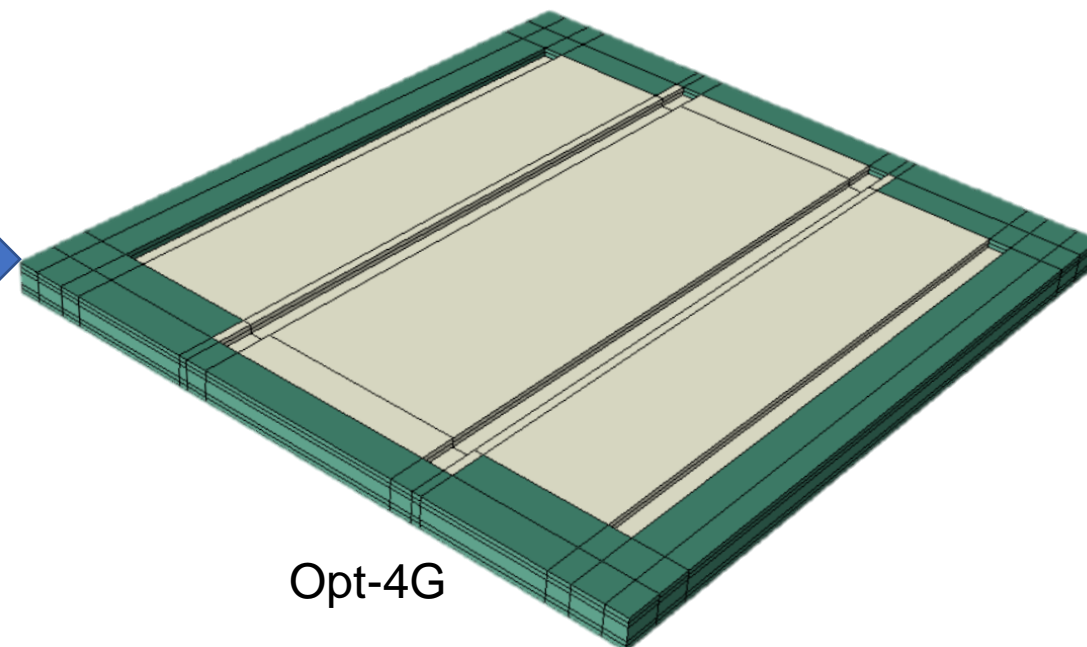
Green : EVA
White : PIB



Fully encapsulated



4 GROOVES



Opt-4G

Design principles:

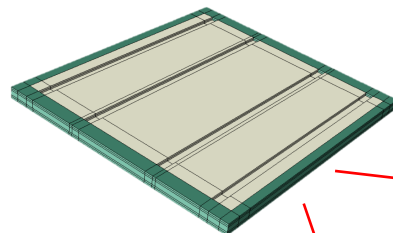
- Frame to stability & avoid creep of soft PIB
- Grooves and corrugation for lower stiffness and increase shear & damping
- Use the contrast of properties to enhance deformation of soft material
- Used the same methodology to optimize prototype pad with Semperit's materials

Digital twin level 2: further design optimization

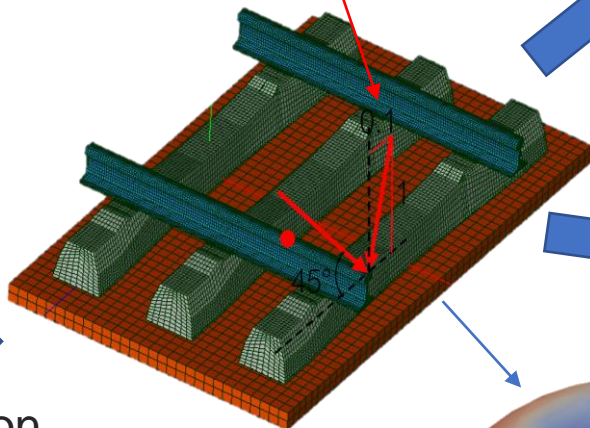
Digital twin approach “level 2”:

Detailed 3D optimization of the pad design

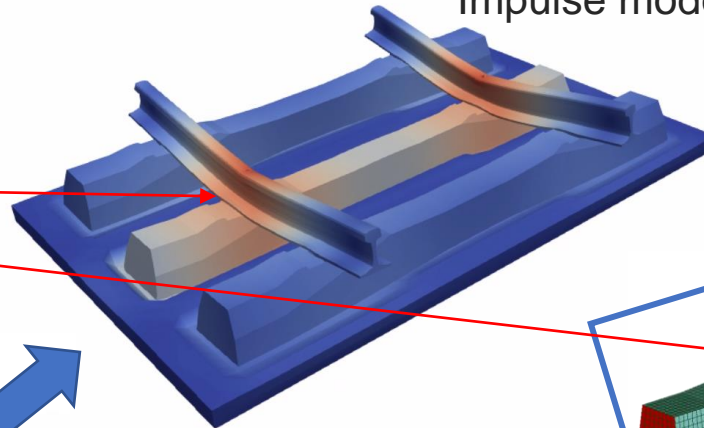
pad design
(3D FEM +
materials)



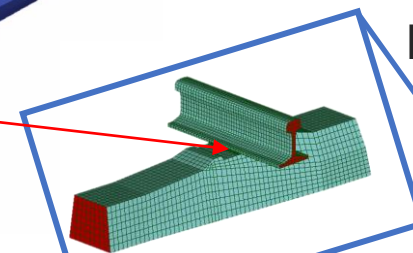
Three sleepers model



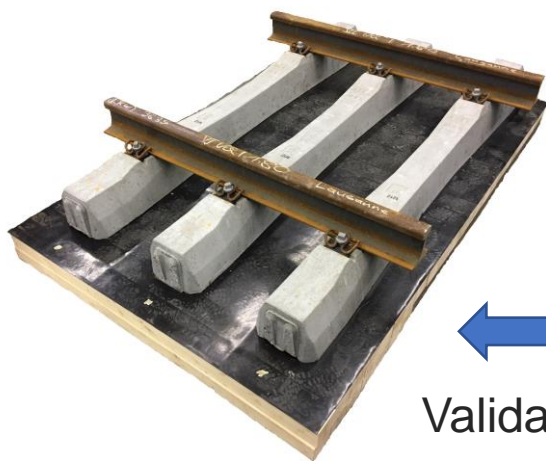
Impulse model



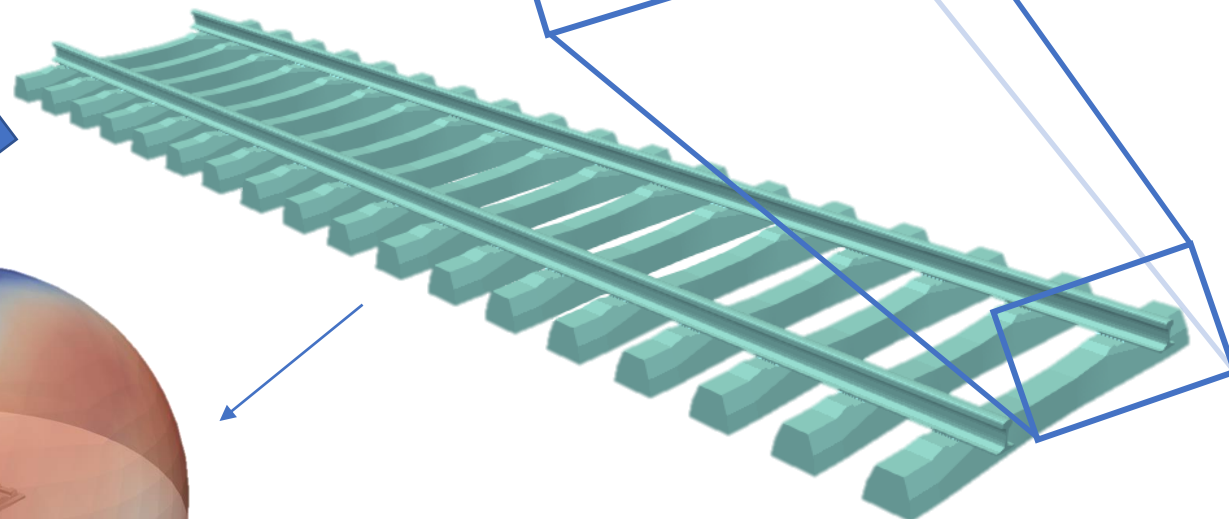
Macro element



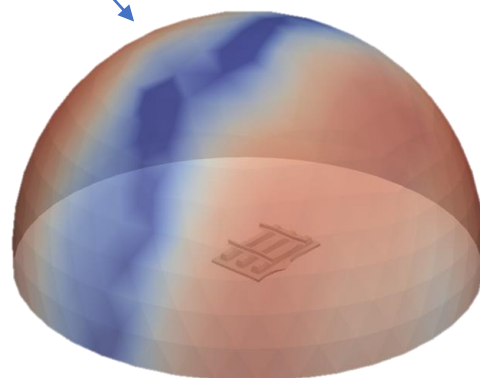
Experimental unit cell



Validation



Large scale track using
dynamic substructuring

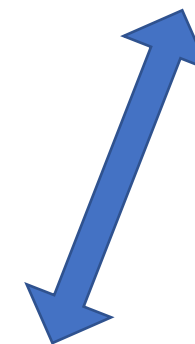
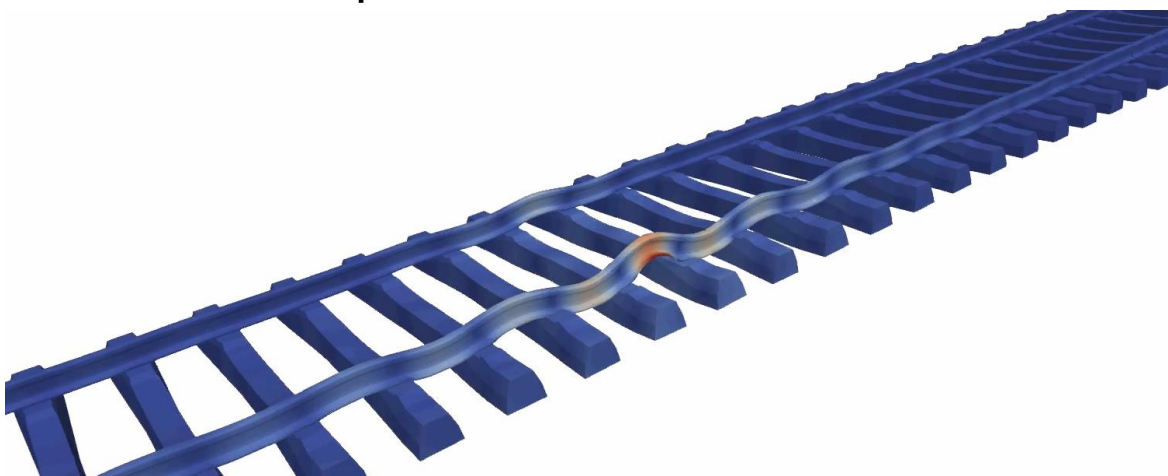


Sound pressure levels estimated with either
the three sleepers model or the multi-sleeper model

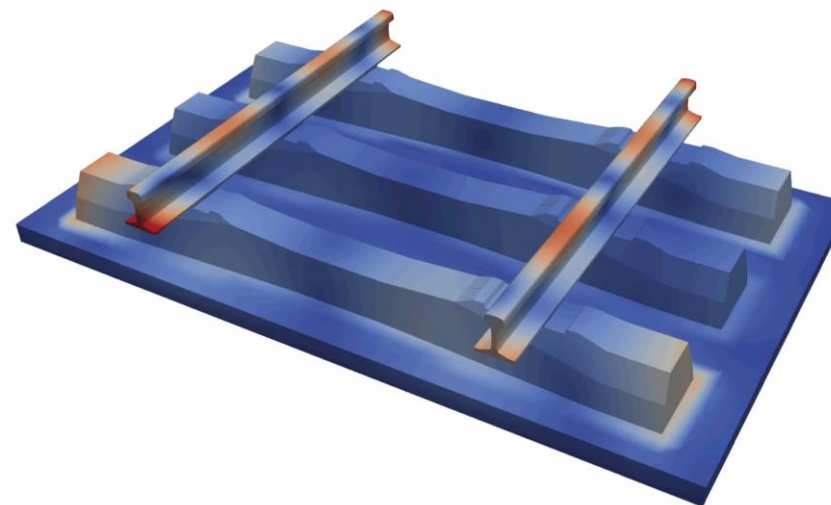
Three-Sleeper & Multi-Sleeper models

- 3D vibro-acoustic simulations
- Frequency spectrum → 300Hz to 1500Hz
- Acoustic pressure field using (monopoles superposition)

- ✓ Actual rail tracks prediction
- ✓ Model improvements → Fast

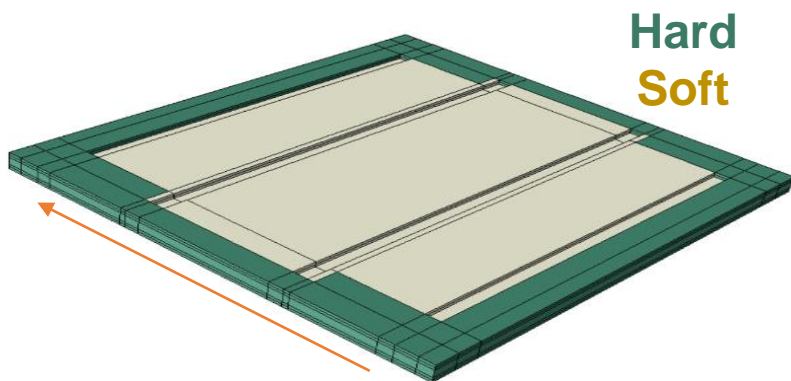


- ✓ Digital twin
- ✓ Calibration
- ✓ Validation

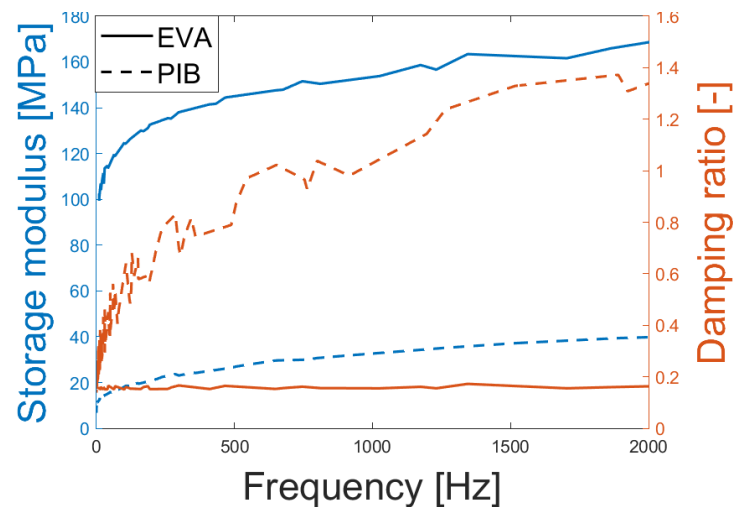


Main inputs/outputs

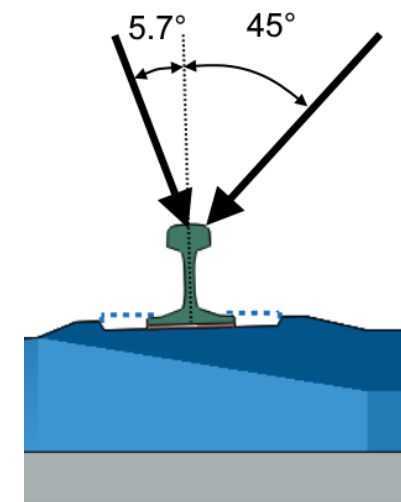
INPUTS



3D pad mesh

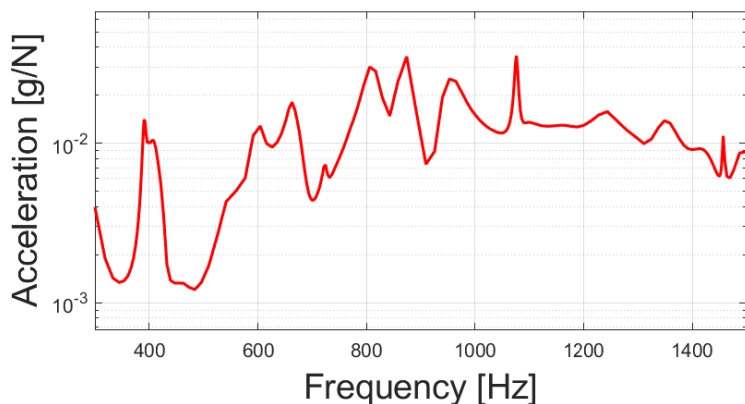


Pad & ballast frequency-dependent materials properties

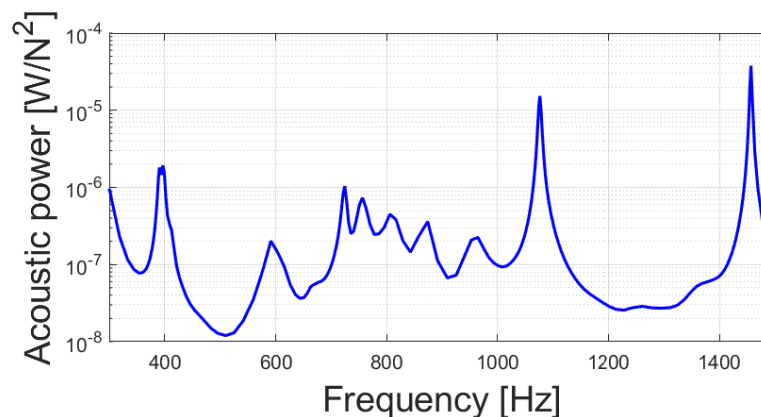


Load direction

OUTPUTS



Rail & sleeper acceleration FRF

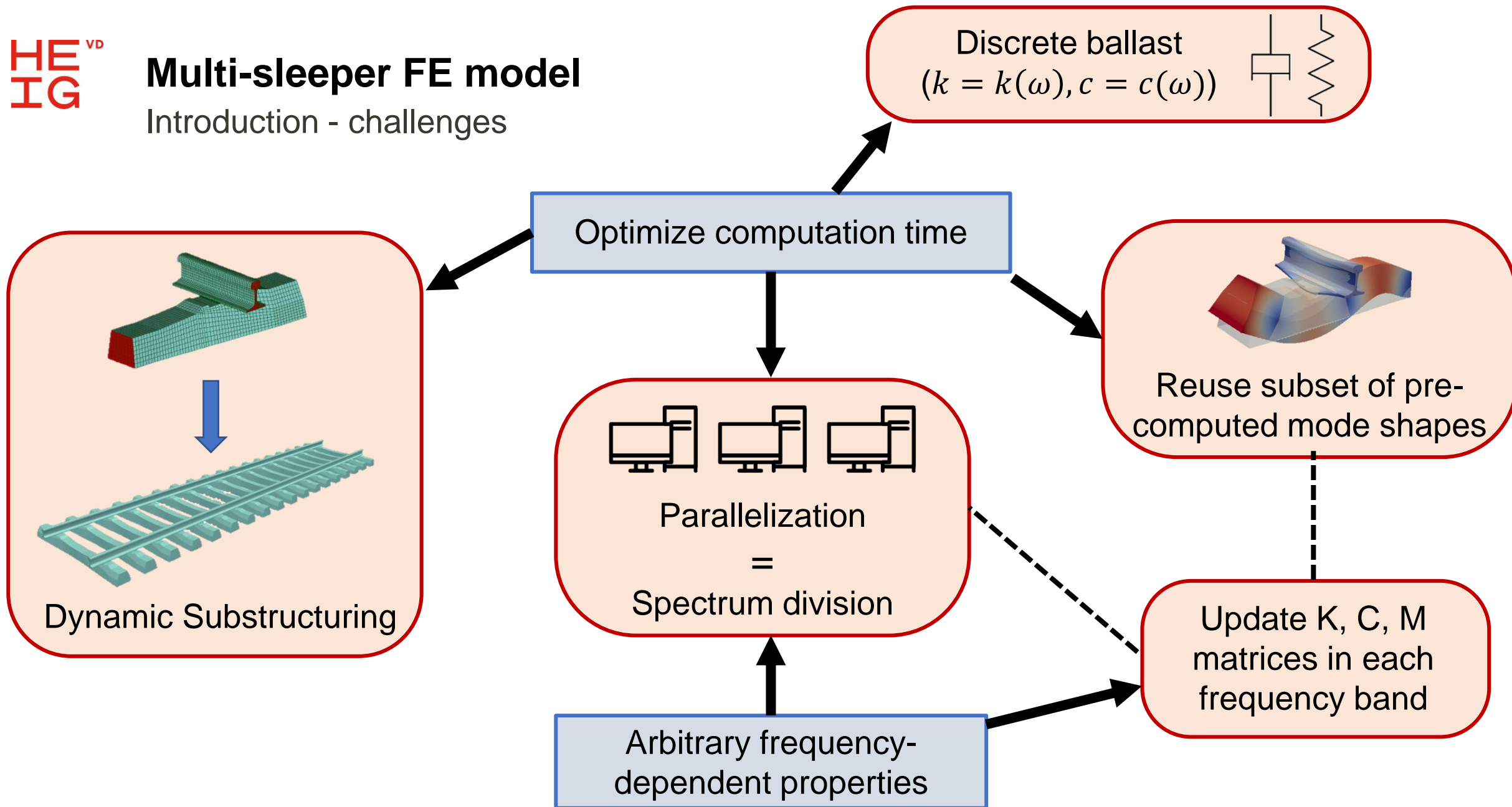


Total radiated acoustic power FRF

$$L_w = \dots \text{ dB}$$

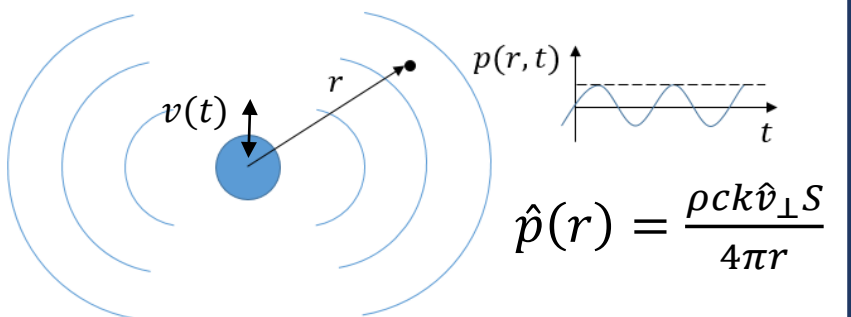
Multi-sleeper FE model

Introduction - challenges

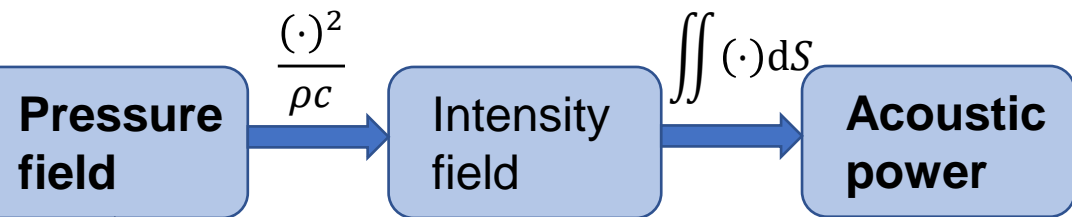
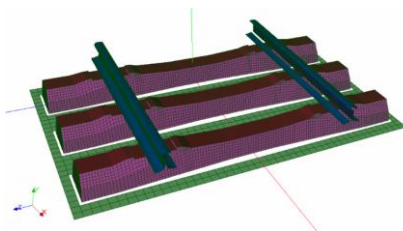


Monopole superposition

Monopole source assumption

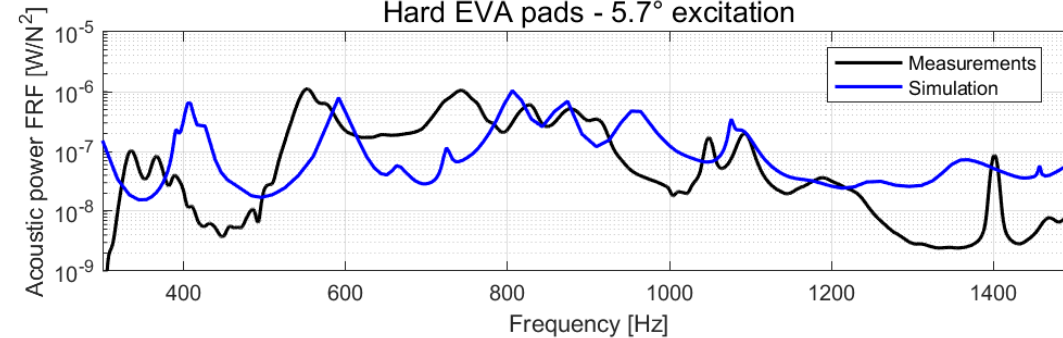


\sum (radiant surfaces contributions)

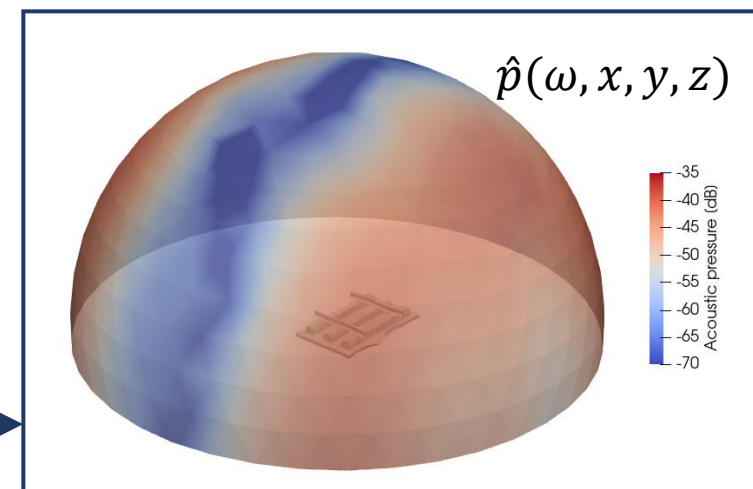
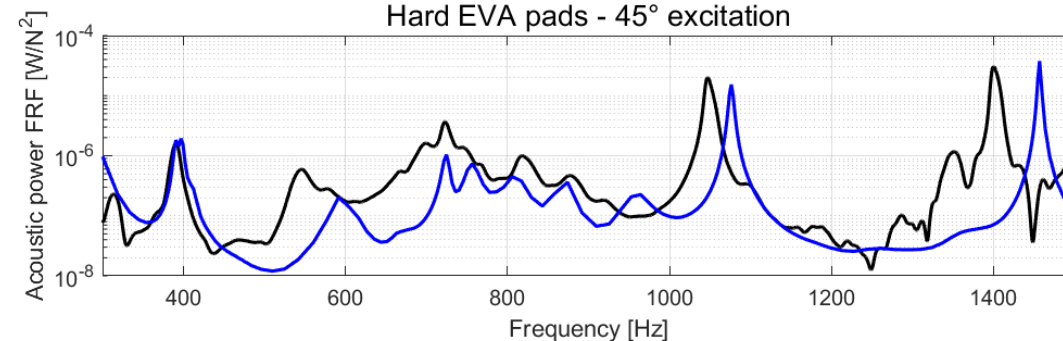


3-sleeper model - acoustic validation

Hard EVA pads - 5.7° excitation



Hard EVA pads - 45° excitation



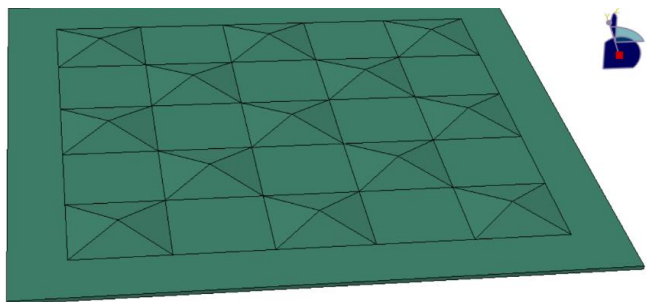
Hybrid pad design using Semperit high damping rubber - Hytrel

Pyramid / shear amplification concept

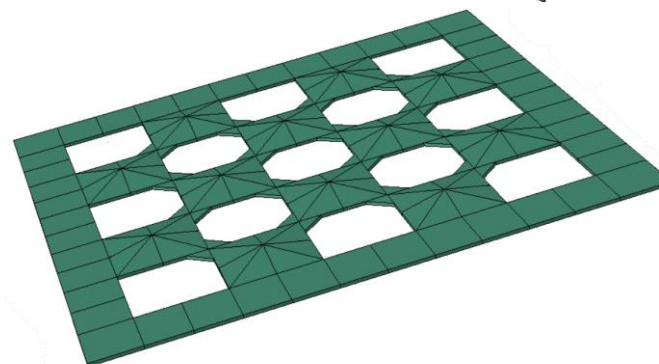
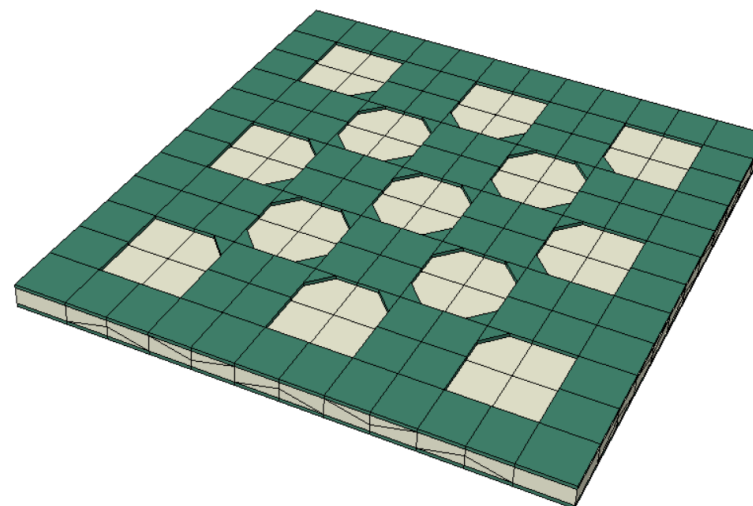
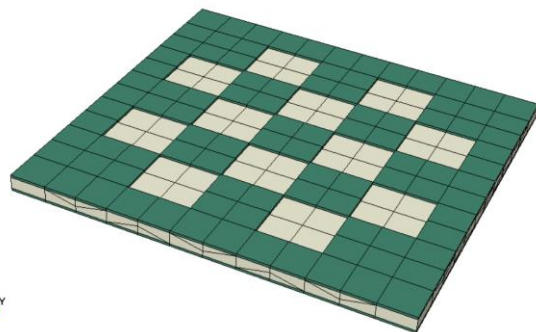
Pad Hybrid08

V3

V1

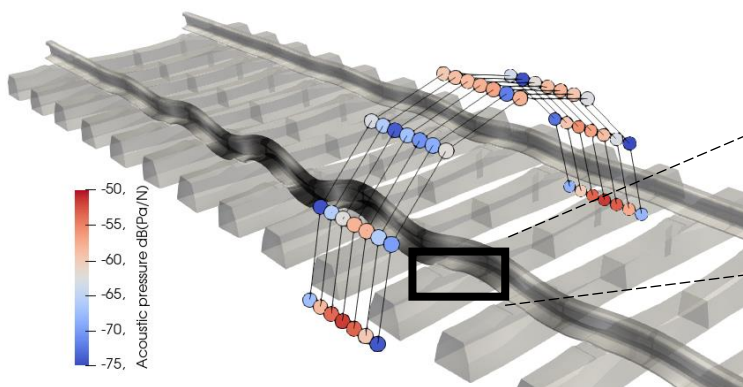


V2

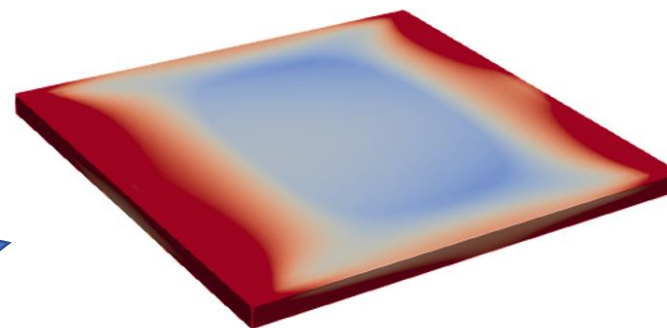


Hybrid pad design using Multi-Sleeper Model

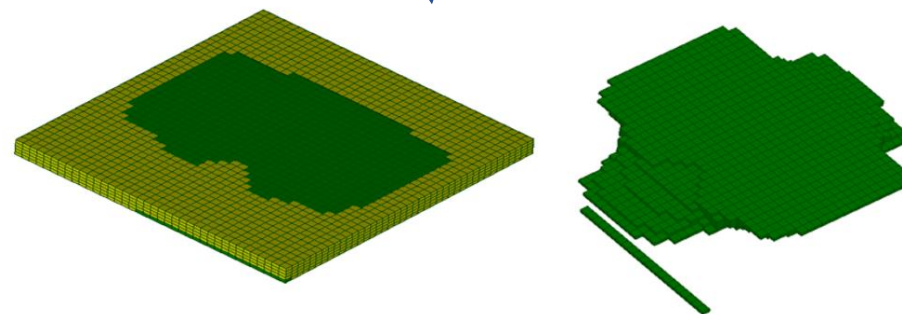
Vibro-acoustic simulation



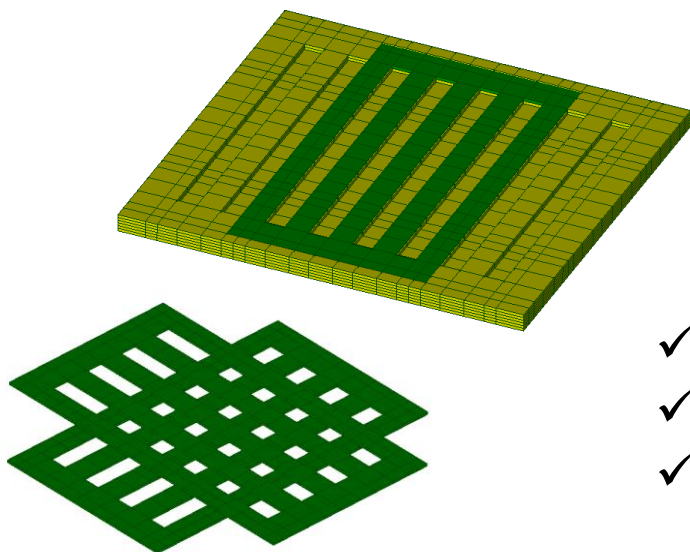
Rail pad deformation field



Place high-damping soft material in large deformation zone



Use stiff material to amplify strain in high damping material



- ✓ Clean CAD
- ✓ Process compatible
- ✓ Grooves → tailored stiffness

Results: Pareto diagrams

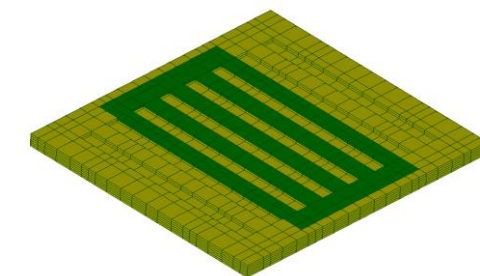
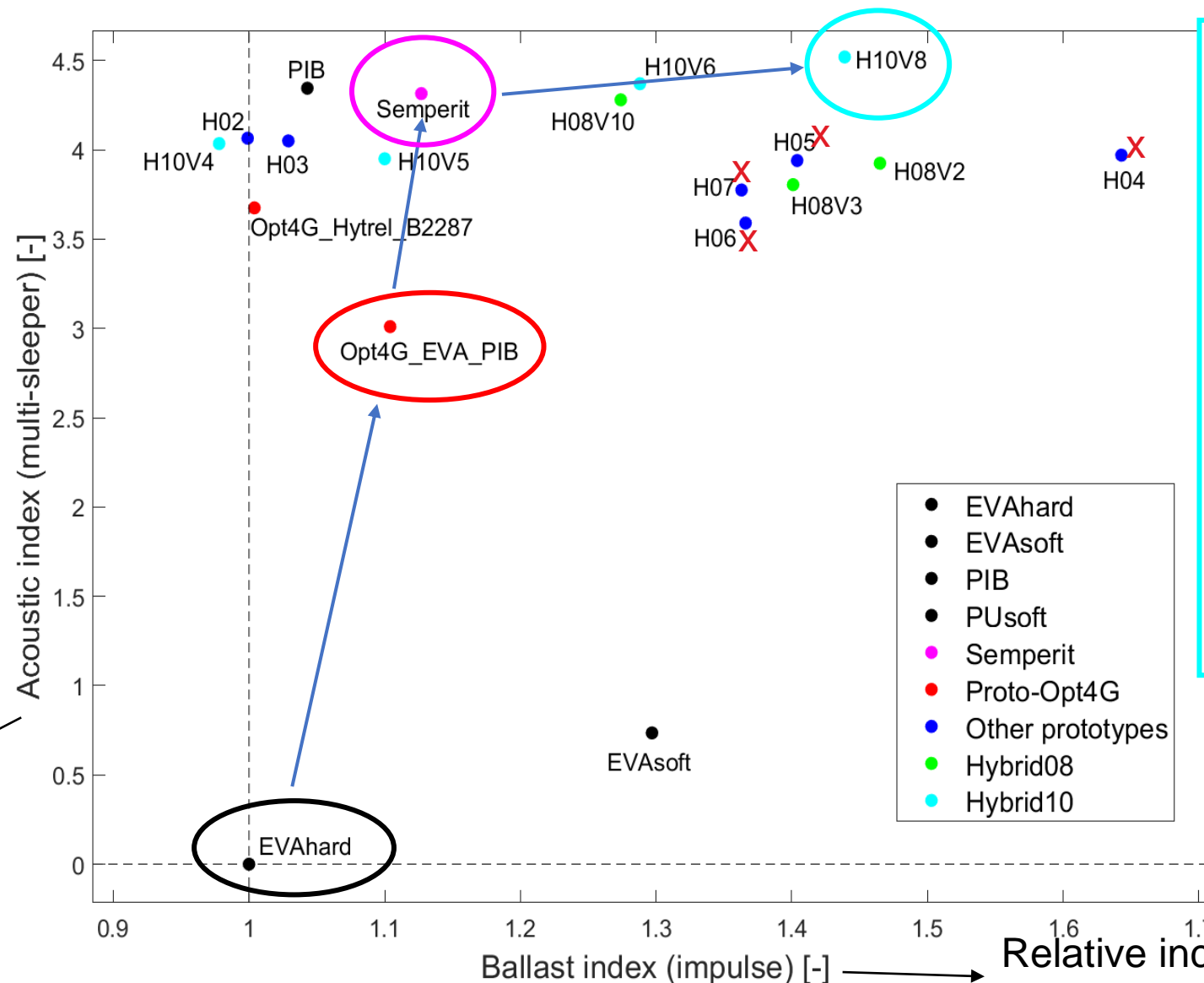
SemperSilent

- ✓ Single-material
- ✓ -4.3 dB (300-1500Hz)
- ✓ 13% ballast protection improvement
- ✓ ~240 kN/mm (static)

Core-Shell EVA-PIB

- ✓ Bi-material
- ✓ -3.0 dB (300-1500Hz)
- ✓ 10% ballast protection improvement
- ✓ ~460 kN/mm (static)

dB noise
reduction



Optimum Hybrid Design

- ✓ Bi-material
- ✓ -4.5 dB (300-1500Hz)
- ✓ 40% ballast protection improvement
- ✓ ~160 kN/mm (static)

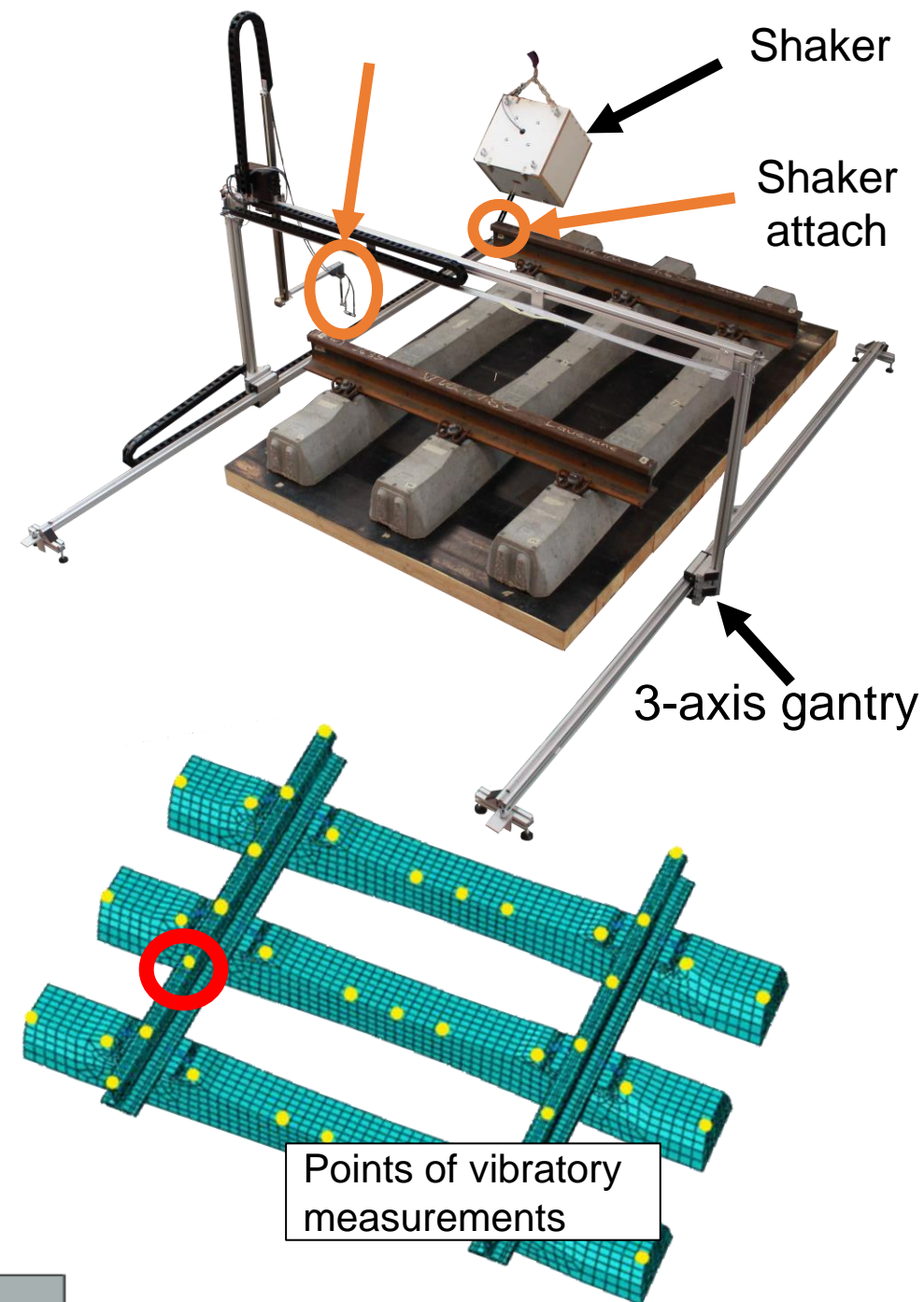
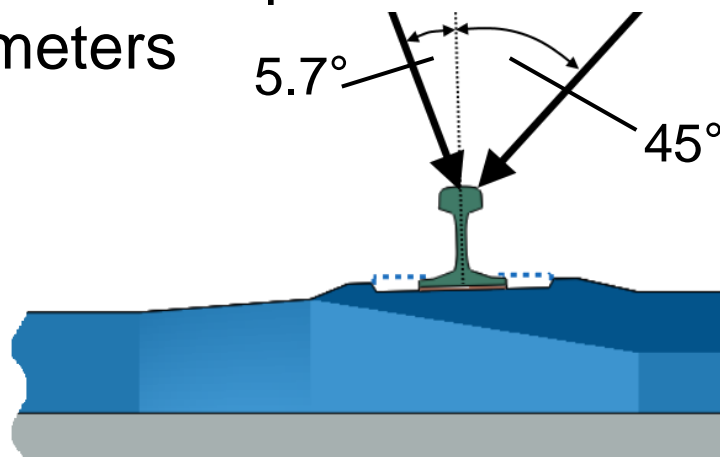
X = fatigue failure or
manufacturing issues

Relative increase of
maintenance interval

Experimental validation & performance evaluation

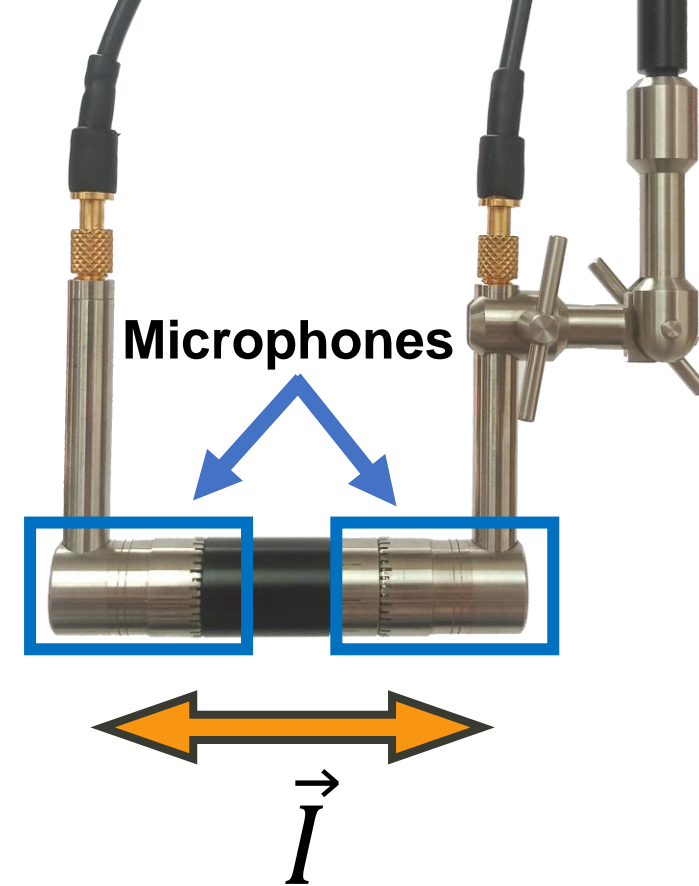
Experimental test bench

- *Three-sleeper cell* consisting of :
 - 2x 60E1 rail segments, 1.8 m long
 - 3x B91 sleepers
 - 12x Vossloh W14 clamps
 - 10 cm-thick wooden ballast substitute
- Excitation by electromagnetic **shaker** attached to the rail, 45° or 5.7° angle
- Semi-automated **3-axis gantry** to move **microphone** for acoustic measurements
- Vibratory measurements performed with 3-axis accelerometers

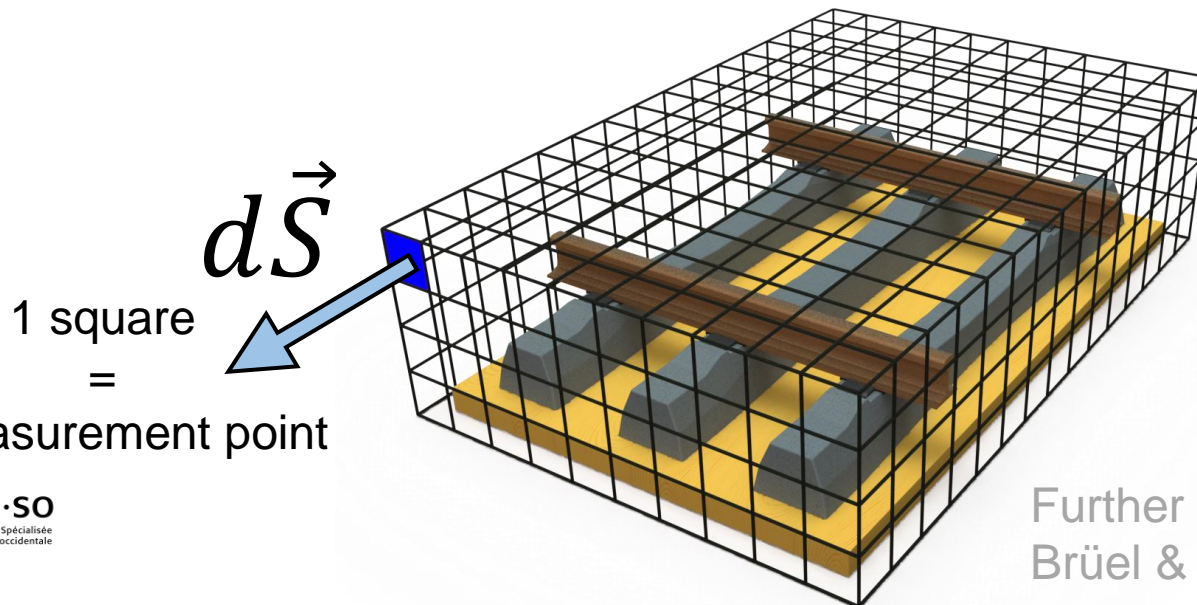


Acoustic measurements : intensimetry

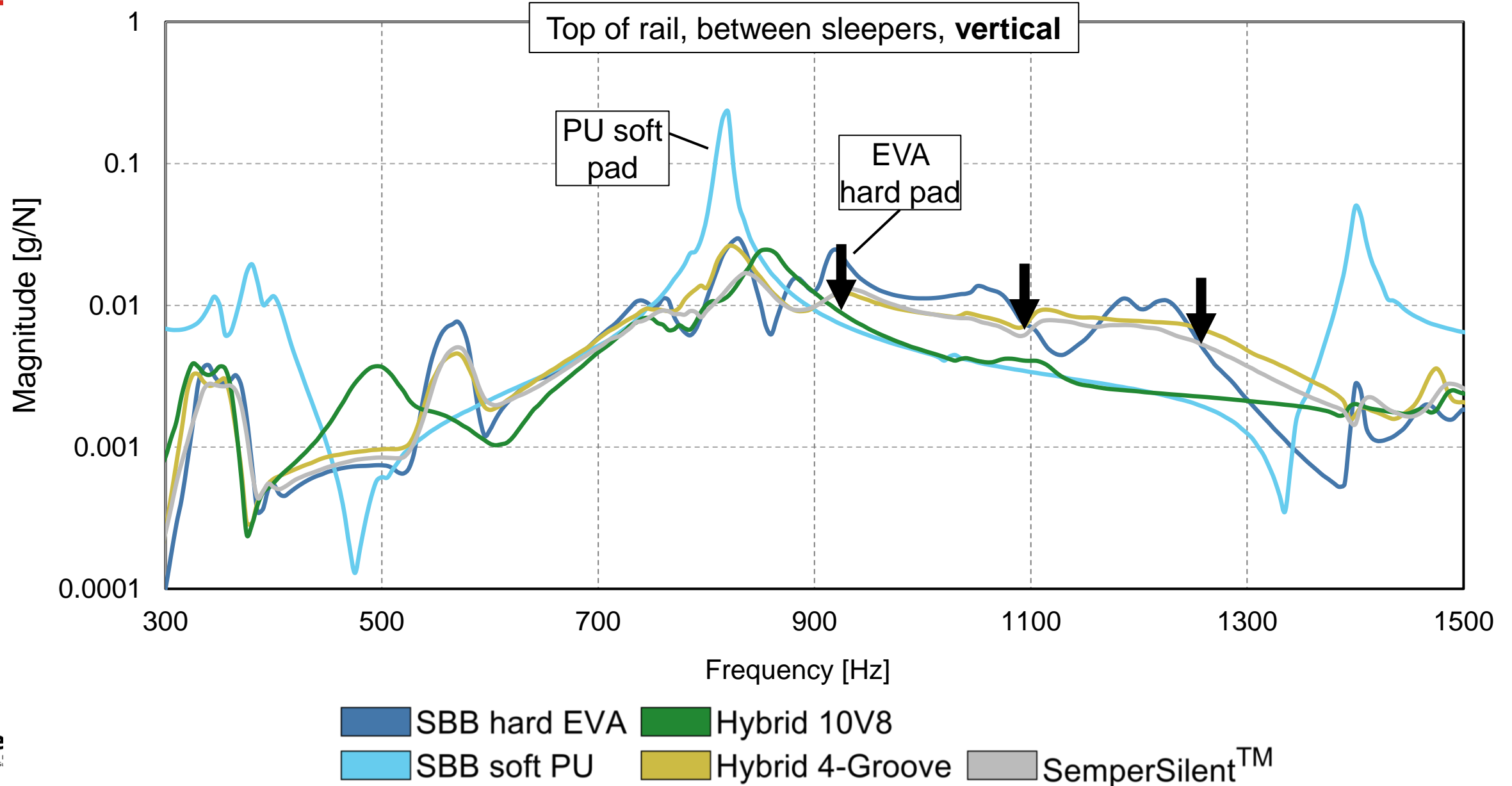
- **Sound intensity** (in W/m^2) measurement
- Using a pair of phase-matched microphones
- Measurement at discrete points evenly spaced on an enclosing surface
- Integration of intensity over the enclosing surface to obtain radiated **sound power** (in W)
- Rail-induced noise is measured



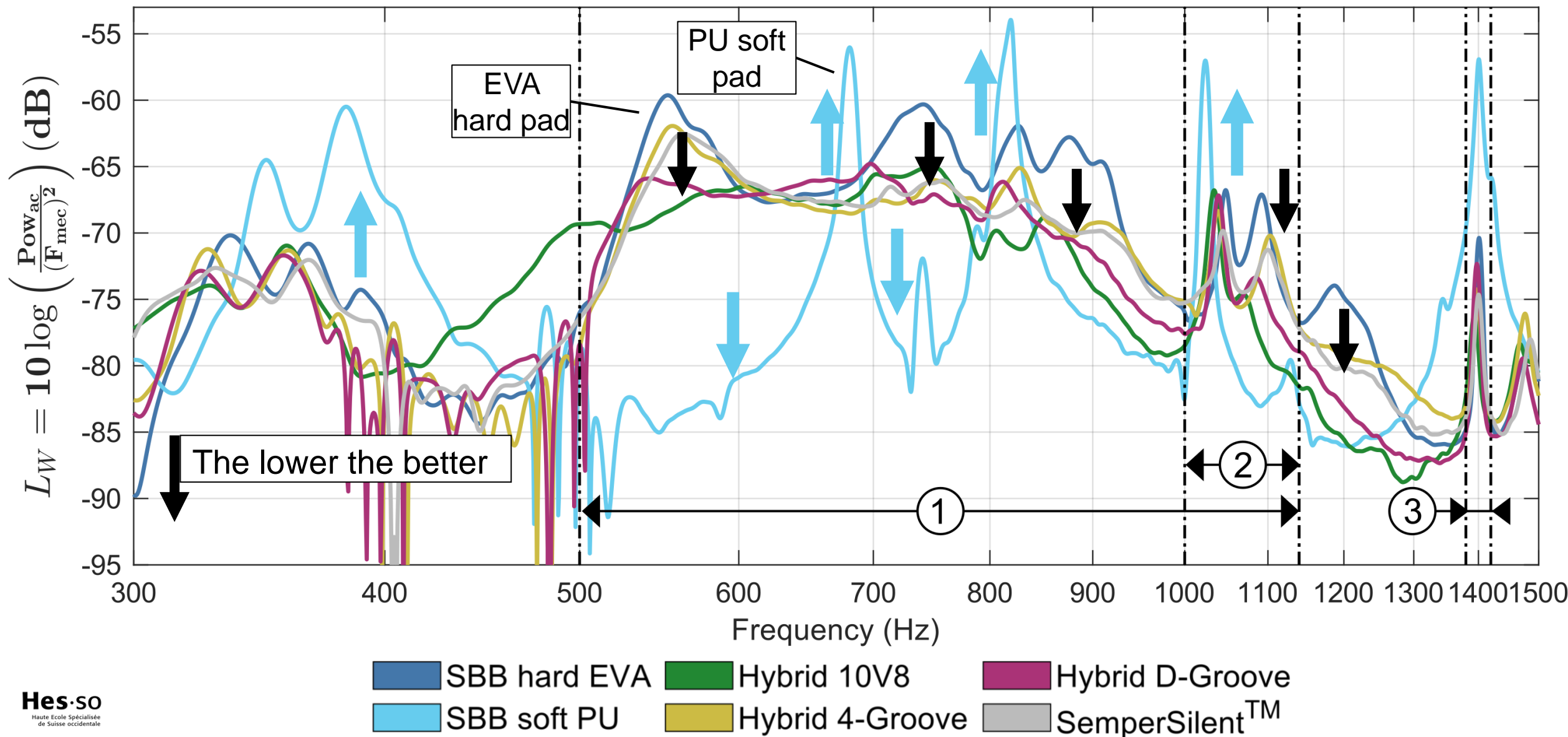
$$\int_S \vec{I} \cdot d\vec{S} = Pow_{ac}$$



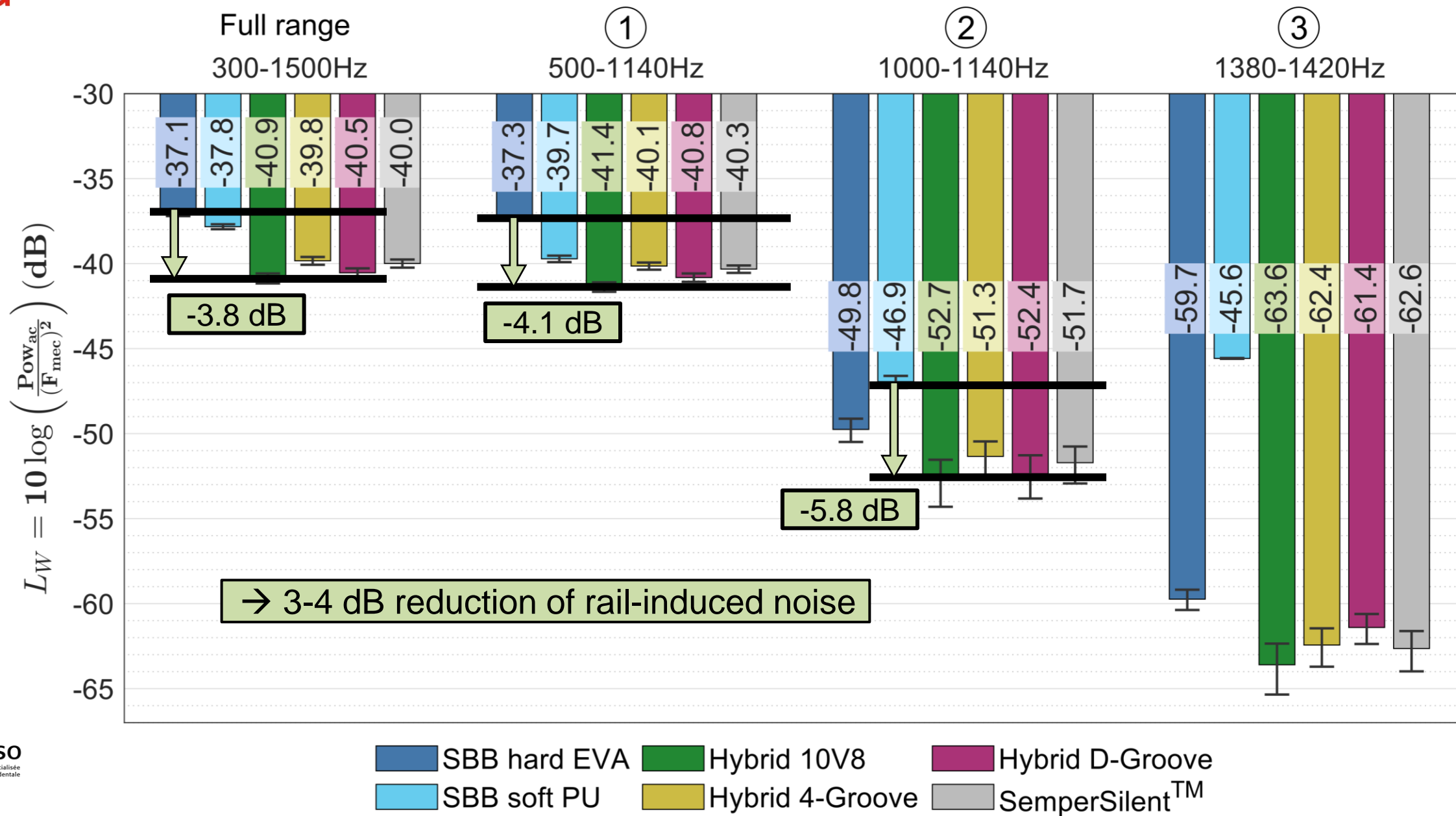
Experimental results – Vibrations, load at 5.7° (mostly vertical)



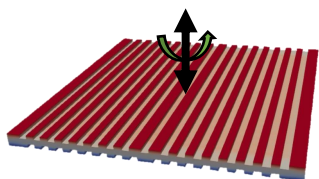
Experimental results – Acoustic , load at 5.7°



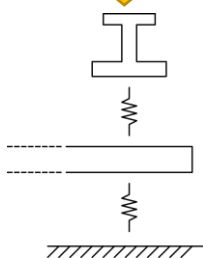
Experimental results – Acoustic, load at 5.7°



Open source rail track modelling toolchain

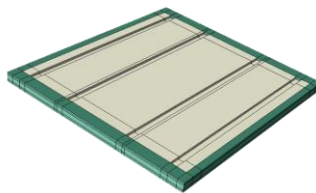


Pad Stiffness Model
Frequency dependent
stiffness and damping

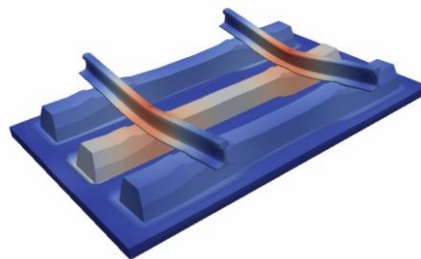
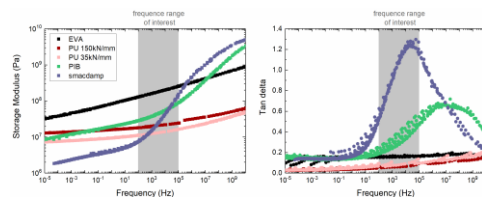


Semi-analytical track model
TDR, noise, vibration

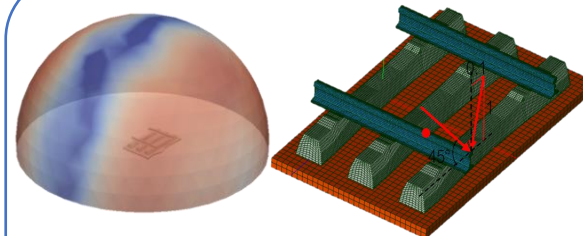
Railpad FE Model
Mesh in Salome MED format



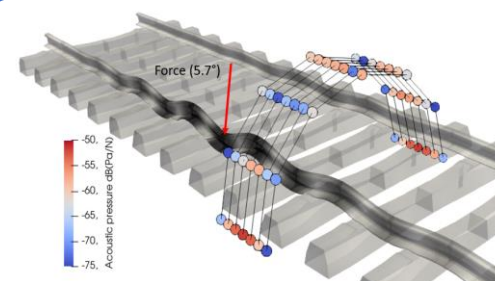
Material properties: pad, ballast, ...
.csv file, space separator



Impulse model
Ballast stress & clamp displacement



Three sleepers model
Vibration & noise radiation



Multi sleeper model
Vibration & noise radiation

Source code, user and installation documentation available at :

<https://github.com/jcugnoni-heig/RailTrackModellingToolbox>

Open source rail track modelling toolchain

The screenshot displays the RailTrackModellingToolbox GUI on a Linux desktop. The main window shows a workflow diagram with icons for Pad Stiffness GUI, Railpad FE Model, Three sleeper model GUI, Multi sleeper model GUI, Impulse Model GUI, and Semi-analytical Track Model GUI. A 'Multi-sleeper model' sub-window is open, showing simulation parameters like Number of modes, Number of sleepers, Load direction, and Default node. The desktop background features a mountain landscape and the text 'CAELinux - Open Source Powered Engineering'.

CAELinux - Open Source Powered Engineering

Conclusion

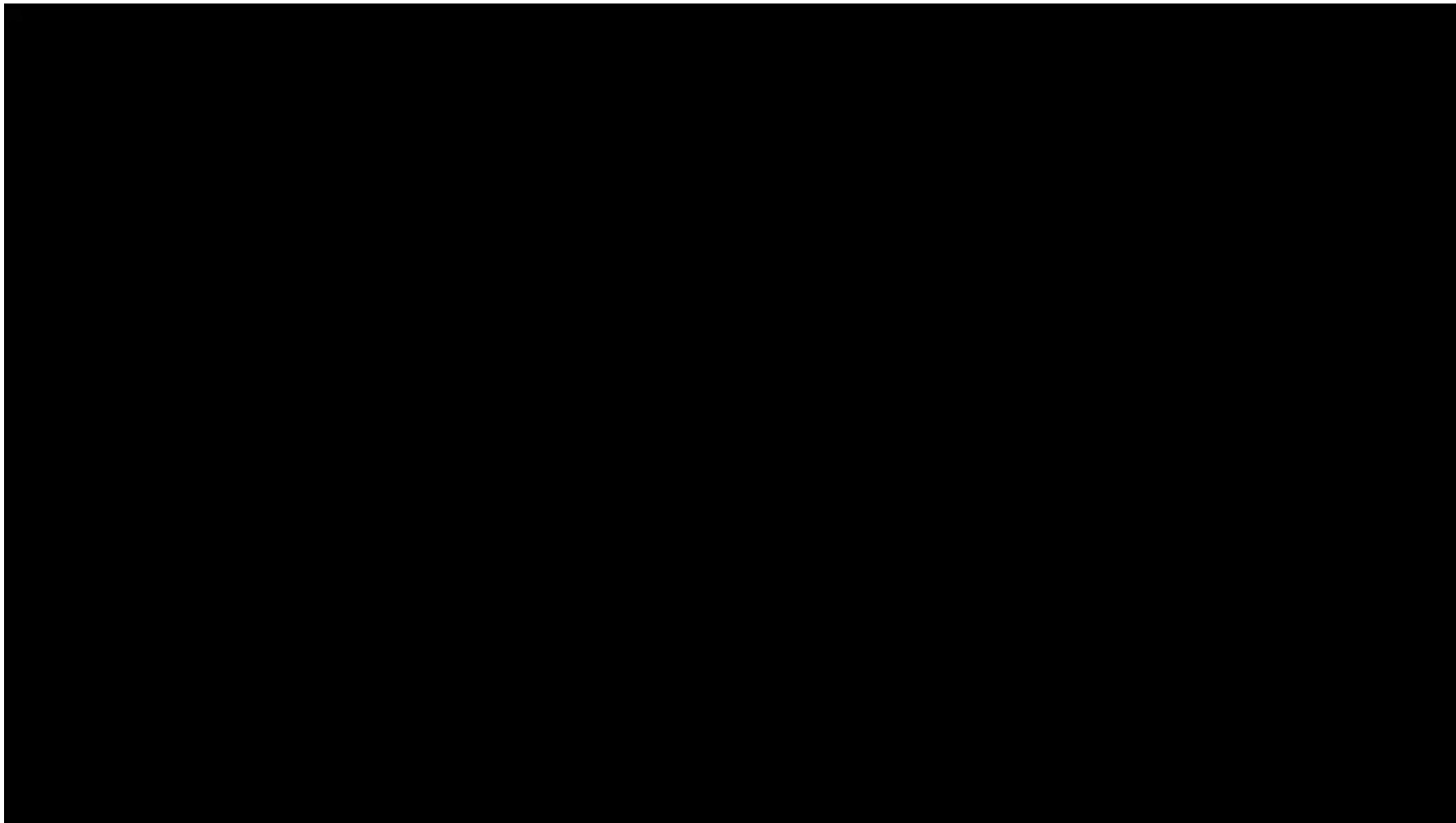
Pad design & optimization

Multiple novel railpad designs using different combination of hard & high damping materials
Noise / ballast protection performance compromise, design guided by Pareto chart
Single material pad optimized with Semperit: good performance / cost tradeoff
Further performance increase using hybrid prototype Hytrel – high damping Semperit rubber
Experimental performance evaluation in line with prediction by models
Rail-borne noise reduction -3-4dB, Maintenance interval + 10-30%

Modelling toolbox

Complete modelling toolbox to evaluate track performance for different pad / material designs
Include USPs & frequency dependent properties of the ballast (EMPA) and materials (EPFL)
Evaluate pad stiffness & damping, radiated noise, vibrations (sleeper, rail), ballast stress & pad / clamp deformations during dynamic axle loading.
Validated across multiple experiments on 3 & 18 sleeper tracks
Published as open source code with detailed documentation

For the story: this is how the « magic » happens...



... with passionate, creative and dedicated engineers !